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"पुराने को छोड नये के तरफ" Jawaharlal Nehru "Step Out From the Old to the New"

मानक

IS 8745 (1994): Methods of presentation of data of physical and mechanical properties of timber [CED 9: Timber and Timber Stores]



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## भारतीय मानक

# लकड़ी के भौतिक व यांत्रिक गुणधर्मों के आरेखों की प्रस्तुतीकरण पद्धतियाँ

## ( पहला पुनरीक्षण )

## Indian Standard

## METHODS OF PRESENTATION OF DATA OF PHYSICAL AND MECHANICAL PROPERTIES OF TIMBER

## (First Revision)

UDC 674.03 : 539.3/.8 (083.54)

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BUREAU OF INDIAN STANDARDS MANAK BHAVAN, 9 BAHADUR SHAH ZAFAR MARG NEW DELHI 110002

#### FOREWORD

This Indian Standard (First Revision) was adopted by the Bureau of Indian Standards, after the draft finalized by the Timber Sectional Committee had been approved by the Civil Engineering Division Council.

Evaluation of basic properties of timber is an important base for establishing design functions of structural timber. For this purpose small clear specimens and specimens in structural sizes are tested according to standard procedures laid down in IS 1708 (Parts 1 to 18): 1986 'Method of testing of small clear specimens of timber (second revision)' and IS 2408: 1963 'Method of static tests of timber in structural sizes'. In order to obtain a good average figure which is truly representative of the species, it is necessary to take samples from different trees and further from different logs. IS 2455: 1990 'Method of sampling of model trees and logs for timber testing and their conversion (second revision)' contains information pertaining to sampling of model trees and logs for timber testing and their conversion for testing' provides information with respect to timber scantling. This standard covers the methods of presentation of data of physical and mechanical properties of timber.

This standard was first published in 1978. Among important modifications, in this first revision the tables for presenting the physical and mechanical properties of timber have been modified to include cleavage (resistance to splitting) and nail and screw withdrawal resistance. Table 3, giving units and scheme for rounding off, has been modified accordingly to take care of these additional properties.

The composition of the technical committee responsible for formulation of this standard is given in Annex A.

For the purpose of deciding whether a particular requirement of this standard is complied with, the final value, observed or calculated, expressing the result of a test, shall be rounded off in accordance with IS 2:1960 'Rules for rounding off numerical values (*revised*)'. The number of significant places retained in the rounded off value should be the same as that of the specified value in this standard.

## Indian Standard

## METHODS OF PRESENTATION OF DATA OF PHYSICAL AND MECHANICAL PROPERTIES OF TIMBER

## (First Revision)

#### **1 SCOPE**

1.1 This standard outlines the methods of presentation of physical and mechanical properties of timber for the purpose of comparison, reduction and adjustment for different design values and utilization for various industrial uses.

1.1.1 It, however, does not include the methods of computation of timber testing data.

#### **2 REFERENCES**

The Indian Standards listed below are necessary adjuncts to this standard:

IS No.	Title
707 : 1976	Glossary of terms applicable to timber technology and utilization (second revision)
1708 (Parts 1 to 18): 1986	Methods of testing small clear specimens of timber (first revision)
2455.1990	Methods of sampling of model trees and logs for timber test- ing and their conversion (second revision)
8720 : 1978	Methods of sampling of timber scantlings from depots and their conversion for testing

#### **3 TERMINOLOGY**

3.1 For the purpose of this standard, definitions given in IS 707: 1976 and IS 2455: 1990 shall apply.

#### **4 PRESENTATION OF DATA IN GREEN** CONDITION

4.1 The tests shall be carried out as specified in IS 1708 (Parts 1 to 18): 1986 and the results shall be presented as given in Table 1 and Table 1A in case of logs selected as recommended in 1S 2455 : 1990. If the material for the tests is taken for depot as recommended in IS 8720: 1978, the results shall be presented as given in Table 2.

4.2 Tables 1, 1A and 2 shall have proper heading and shall be self-explantory and indicative of conditions and limitations of the results.

4.3 Tables 1, 1A and 2 shall include the details mentioned in 4.3.1 to 4.3.5.

#### 4.3.1 Average

The average of all sticks in a bolt or tree shall be called as 'tree average'. Similarly, the average of all sticks in a scantling shall be called 'scantling average'. The average of 'tree average' or 'scantling average' shall be called 'species average' of the locality. Usually the 'species average' of the locality shall be reported in Tables I, 1A and 2 under respective conditions of test, that is, green, kiln-dry, air dry or at any moisture content ( see 5 ).

4.3.2 While reporting the results, the values shall be rounded off according to the scheme mentioned in Table 3.

4.3.3 Besides physical and mechanical properties the following details shall also invariably be recorded:

- a) Locality,
- b) Rings per cm,
- c) Size of the logs (in case of logs),
- d) No. of trees or scantlings, and
- e) No. of specimens for individual tests.

4.3.4 As in green condition the moisture content has no influence on strength properties, the average moisture content of all the tests shall be reported.

#### 4.3.5 Measure of Variability

For all data in timber testing a measure of variability shall be given. The scheme given in Table 4 is recommended for reporting the measure of variability for different purposes.

#### **5 PRESENTATION OF DATA UNDER DRY** CONDITION

5.1 All the 'tree average' or 'scantling average' in respect to strength in the dry condition shall be adjusted to 12 percent by the formula:

$$\frac{S_{12}}{S_{g}} = \left(\frac{S_{d}}{S_{g}}\right)^{\left(\frac{f-12}{f-d}\right)}$$

where

- $S_{12} =$  strength required at 12 percent moisture content;
- $S_d$  = strength observed at *d* percent moisture content in dry condition, that is, moisture content below fibre saturation point;
- f = fibre saturation point;
- $S_{\rm g}$  = strength in green condition; and
- d = observed moisture content in dry condition.

**5.2** If the fibre saturation point is not available the strength value (tree or scantling average) shall be reduced to 12 percent by the formula:

$$S_{12} = \frac{dS_d}{12}$$
, provided (12 - d) is within a limit of +2 percent

5.3 The impact bending values or values determined under dynamic condition shall not be adjusted to 12 percent but averaged and reported at that moisture content.

5.4 While averaging the test data from specimens of a single bolt or scantling conditioned to a given moisture content care shall be taken that the moisture content shall not vary by more than 1 percent. 5.5 When it is required to compare data in different conditions (say green and dry), care shall be taken that the data correspond to matched samples of equal numbers in each condition. Alternatively, it will be necessary to adjust data of one condition to suit the data in other condition by giving due weightage to the number of samples tested and by evaluating the average ratio of the values in the condition from known matched material.

#### Example:

Let the species average of five bolts in the green conditions be given by K and that of five individual bolts in the green condition by  $S_1$ ,  $S_2$ ,  $S_3$ ,  $S_4$ , and  $S_5$ . If values of only three matched bolts in dry condition are known as  $S_1'$ ,  $S_2'$  and  $S_3'$ , then the species average K' in the dry condition for all the five bolts is given by:

$$K' = K \times \frac{1}{3} \sum_{i=1}^{3} \frac{S'}{S}$$

5.6 An improvement factor which is the average percentage of improvement of strength values from green to dry condition (at 12 percent) shall also be reported.

Table 1 Physical and Mechanical Properties of Timbers in Green (G) and in Air Dry ( AD ) Condition ( Log Selected According to 15 2455 : 1990 )

(Clauses +.1, +.2, 4.3 and +.3.1)

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51 Ne.	Species and Trade Name	Locality From Where Tested	Consign- ment No.			· .	Speci Grav Base on Mi Over-	đe ity id Dry		P	Shrink ercent (a Over	age Grees I-Dry		Sénci ;	e Bend	ing Vork ju	•] mm•		Imp	es Bene	ling		Compi Parsi Gr	ession lei 10 lin	Compression Perpendicula to Grain	Le La Be	Hardae ad in N ( Embed on Diamo ill to Hail	kgf ) 1:128 rter f Dia	Shear Paraile to Grai	Te Per G	rasian rpradi- inr to rain	Clean ( Restau Spiim	vage Lace to Lag )	Tensi	o Para Grain	lel ·	Torsi	iop		Remarks
				Vilua	No. of Tees No. of Tees 	kurgt per cur	Volucie, al Trut	Volume treating	Manue (autral percent	Main true a	Kadaal 	Vujustetin	blire Stress at Havie Linon, Nfmm <sup>2</sup> - kgf/sm <sup>2</sup> )	$M$ -dottes of R options, N/mm2 , kgf ( $\omega^{\rm R}$ )	Modulus of Elestrony, Name (1960) kgl/cm <sup>4</sup> ( 	To Llaste I unit	Do Manufacture 1	hore Sirer at Elanis, Lunds, Namé (Agl 1m².)	Maaning Hugha of Drop of 22 7 by Hammer, non	M. d. n.d. si P. haroate - Nymurt y Peerlijst end y	Ասլեւս Լետոս Լոստ, ա ԳԼաստ∙ւնբեշտ շա <b>Բ</b> է	Bantinan Week Maratada) (Agl ette) 	Countriance Stream at histor Lonor, Stand. 1 Marcar 7	( *maile the state of states a state of the light maile and so	նանգերութ է ներթես է լուս եստնեն, աստ՝ է եցի ան <sup>1</sup> է		Ka kel		Kadadi Ximmala (agdikada)	latigation of the second of th	Tareenang, Se te u te e te fauf a	kudadi (i. m.)	ر طائمه عنه عها بالحدم معمار المقدم ومراجع	Li muti, Svrens at Limite, Limite, Namite (glam).	Mammud Trunce Stree 2: som tyglicut )	Michael (Hastrate, Michael (Hamble) and grant (	strat strate at a tarta strate. Strate is the strate of t	։ Գերեն են ե	A stage 'Ye' Pouts	
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#### Table 1 (A) Nail and Screw Withdrawal Resistance

(Clauses 4.1, 4.2, 4.3 and 4.3.1)

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SI No.	Species	Locality From	Consign- ment No.	Values						Na	il/Scre	w Wit	hdraw	al Res	istance	N ( k	gf)					
		Where Tested	No.		Nail	l/screw ar	Condi driven id pull	iion A in gree ed at oi	n cond nce	ition	Nai	l/screw and j	<i>Condi</i> driven pulled i	<i>tion B</i> in gree n dry c	en cond conditic	ition m	Nai	l/screw a	<i>Condil</i> driven and pul	ion C in dry led at o	condit once	ion
						Nail			Screw			Nail			Screw			Nail			Screw	
					Radial	Tangential	En d	Radial	Tangential	Ead	Radial	Tangentia l	En d	Radial	Tangential	End	Radial	Tangenti a l	End	Radial	Tangential	End
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23
				Average Maximum Minimum																		
			2																			
			1							: 									<u> </u>			

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#### Tuble 2 Physical and Mochanical Properties of Timbers ( Scanting: Selected According to 13 8720 : 1978 ) ( Gresss 4.1, 4.2, 4.3 and 4.3.1 )

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		Locality From	Canadigae	Values		1	Special Gravit	<b>1</b>				64	ntia Be	-Mag			Impact Beading				Compression Parallel to Grain			Gempressian Perpendiquiar	Hart N (b	Hardnoss Load in N (hgf) to Embed		ardness Load in Shear (hgf) to Smbed Parallel		Te	Tension Perpendi-		Cleavage Resistance to Sulition		renge Tension ansee to Parsilei tilag to Grain		Tension Tornion Parallei to Grain				na Nail Withdrawal Screw Resistance Withdrawal Resistance			Roman	- <b>k</b> .s			
	Treade Manage	· Tanad	No.				Hased Mase, Oven-D and							Work IQ { kgf q	ni j/m ni cm²	5							Unit				120 on Half	Dia- Dia Dia		47918	G	rain										-,						
					No. of Jerenings	Rings per cm	Vulume, si Tosi	Valutaa, Over-Dry	Malature Guateat, Petcaat	Muu ia hgim'	Fibre Stress at Ekastic Limit, N/mm <sup>4</sup> ( kg(;cm <sup>0</sup> )	Modulus of Rupture, N/mae <sup>4</sup> ( <b>hg</b> (fcm <sup>4</sup> )	Modulus at Elasticky, Njasm' ( 1 000 tgficm' )	To Blastic Limit	jo Marjøum Load	Total	Fibre Strew at Elastic Limit, N/mai <sup>1</sup> ( hgf/cm <sup>0</sup> )	Marimum Height of Drop of 22.7 ig Hammer, me	Modulus of Elesticity, Nimma ( 1 000 hgljcm <sup>a</sup> )	Work to Elestic Limit, 10.8 J/mm* ( kgf cm/cm* )	Brittleness Work Absorbed, ] ( hgicm" )	Compressive Stress at Etastic Limit, N/mma ( hgf/cen <sup>4</sup> )	Maximum Cambing Strees, N/mm <sup>a</sup> ( kgf/cm <sup>a</sup> )	Modulus of Elasticity, N/mm <sup>4</sup> ( 1 u00 kg/cm <sup>4</sup> )	Compressive Stree at Elastic Limit, Name" ( left/car)	Redial	Tagential	End	Badial, N/mur <sup>6</sup> ( kgf/cm <sup>3</sup> )	Tagential, N/mm² (Lg()cm² )	Radia), N/mmª ( k@(/cm² )	Taagential, N/mm <sup>a</sup> ( Lg(/cm <sup>a</sup> )	Kadial, N/mm Width ( kgf/cm Width )	Tangencial, N/mm Width ( hgl(cm Width )	Tentile Stress at Elastic Limit, Nimm'   hgficm' )	Masimum Trasile Stress, N/mus" ( kgi/cast )	Modulus of Elasticity, Nimm <sup>a</sup> ( ) 100 kg/cm <sup>a</sup> )	Shear Stress at Etastic Limit, N/m.m <sup>3</sup> ( kg(f.cn. <sup>3</sup> )	Maximum Shear Strees, N/munt ( hgf/cm <sup>4</sup> )	Mudulus of Rigidity, N/mm <sup>1</sup> ( 100 kgf.cm <sup>1</sup> )	Radial, N ( 186)	Taugential, N ( kyf )	Ead, N ( kgf )	Kadial, N ( Lgf )	Taugential, N ( kgf )	Ead, N ( Lgf )	(	
-	2	3	+	5	•	7	8	9	10	u	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	39	54	35	36	37	38	39	40	41	+2	+3	44	45	46	47	+8	
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### Table 3 Units and Scheme for Rounding Off Numerical Values

(Clause 4.3.2)

Sl No.	Property	Unit	Scheme of Rounding Off
(1)	(2)	(3)	(4)
i)	General:		• • •
	Average diameter of logs	mm	Nearest integral figure
	Specific gravity		Correct to 3 places of decimal
	Moisture content	Percent	Correct to one place of decimal
	Mass	$kg/m^3$	Nearest integral figure
	Shrinkage	Percent	Correct to one place of decimal
ii)	Static Bending:		
	Fibre stress at elastic limit and modulus of rupture	N/mm <sup>3</sup> ( kgf/cm <sup>2</sup> )	Nearest integral figure
	Modulus of elasticity	$N/mm^2$ ( 1 000 kgf/cm <sup>2</sup> )	Correct to one place of decimal
	Work to elastic limit	10 <sup>8</sup> J/mm <sup>3</sup> ( kgf cm/cm <sup>3</sup> )	Correct to 3 places of decimal
<b>;;</b> ;)	Work to maximum load and total work	10 <sup>-3</sup> J/mm <sup>3</sup> ( kgf cm/cm <sup>3</sup> )	Correct to 2 places of decimal
111)	Fibre stress at elastic limit	$N/mm^2$	Nearest integral figure
	Maximum height of drop	( kgi/cm <sup>-</sup> )	Nearest integral forum
• •	Modulus of elasticity	$N/mm^2$ ( 1 000 kgf/cm <sup>2</sup> )	Correct to one place of decimal
	Work to elastic limit	$10^{-3} \text{ J/mm}^3$ (kgf cm/cm <sup>3</sup> )	Correct to 3 places of decimal
	Brittleness	J (kgf cm )	Nearest integral figure
iv)	Compression Parallel to Grain:		0
	Compressive stress of elastic limit and maximum crushing strength	N/mm <sup>2</sup> ( kgf/cm <sup>2</sup> )	Nearest integral figure
	Modulus of elasticity	N/mm <sup>2</sup>	<sup>~</sup> Correct to one place of decimal
V)	Compression Perpendicular to Grain:	$(1\ 000\ kgf/cm^2)$	
	Crushing stress at elastic iimit	$N/mm^2$	Nearest integral figure
	Umulance	$(kgf/cm^2)$	
VI)	Badial		
	Tangential	N (leaf)	Nearest integral figure
	End	ta ( rgi )	
vii)	Shear:		
	Radial	N/mm <sup>2</sup>	Correct to one place of desired
	Tangential	$(kgf/cm^2)$	Confect to one place of decimal
viii)	Tension Perpendicular to Grain:	· -	
	Radial	$N/mm^2$	Correct to one place of decimal
	Tangential	$( kgf/cm^2 )$	-
ix)	Tension Parallel to Grain:		
	Tensile stress at elastic limit	$N/mm^2$	Nearest integral figure
	Maximum tensile stress	( sgi/cm- )	
	Modulus of elasticity	$N/mm^2$	Correct to one place of decimal
x)	Cleavage Resistance:	(100 Agi/on )	
	Radial	N/mm width	Nearest integral figure
	Tangential ∫	( kgf/cm width )	
xi)	Torsion :		
	Shear stress at elastic limit	$N/mm^2$	Correct to one place of decimal
	Maximum shearing strength $\int$	(kgf/cm <sup>2</sup> )	
	Modulus of rigidity	N/mm <sup>2</sup> ( 100 kgf/cm <sup>2</sup> )	Correct to one place of decimal
xii)	Yo (Intersection-point)	Percent	Correct to one place of decimal
xiii)	Nail and Screw Withdrawal Resistance	N (kgf)	Nearest integral figure

### Table 4 Scheme for Measure of Variability

(Clause 4.3.5)

Sl No.	Average	Measure of Variability
(1)	(2)	(3)
i)	When sticks are taken from a lot for testing the lot average of all sticks shall be repor- ted	Range of observations, that is, maximum and minimum value of all the observations in a test shall be given as measure of variability
ii)	When the data is collected from a parti- cular locality the species average of the locality shall be given	Standard deviation or coefficient of variation or both shall be given as measure of variability. It shall be calculated as follows:
		a) When five or more trees or scantlings are tested from the locality, tree or scantling average shall only be considered for calculat- ing standard deviation or coefficient of varia- tion
		b) However, if less than five trees or scantlings are tested from a locality, all the observations in a test shall be considered for calculating standard deviation and coefficient of variation of the property
iii)	For the data of entire geographical region, the species average of the region shall be reported	Standard deviation or coefficient of variation or both shall be given as measure of variability. It shall be calculated as follows:
		a) These shall be calculated from the tree or scantling averages if less than five different localities are involved in the region
		b) However, if five or more localities are invol- ved in a region the standard deviation or coefficient of variation shall be calculated from the locality averages only

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#### ANNEX A

( Foreword )

#### **COMPOSITION OF THE TECHNICAL COMMITTEE**

Timber Sectional Committee, CED 9

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(Alternate) CHIEF CONSERVATOR OF FORESTS

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JT DIRECTOR, CE (TM) ( Alternate )

DY DIRECTOR OF NAVAL ARCHITECTURE

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Director General, BIS ( Ex-officio Member )

Secretary

SHRI SANJAY PANT Assistant Director ( Civ Engg )

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SHRIS, S. RAJPUT

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